h)

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- 1. A dividing wall column divided in the middle region into a feed section and an offtake section by a dividing wall and having as segments
- a) an upper column region,
- b) an enrichment section of the feed section,
- c) a stripping section of the feed section,
- d) an upper part of the offtake section,
- e) a lower part of the offtake section,

a lower column region,

- f) an intermediate region of the feed section,
- g) an intermediate region of the offtake section and
- where the dividing wall is located vertically between the segments b) and d) and between the segments c) and e), the segments b), d), c) and e) have separation-active internals and the cross-sectional area A_b of the segment b)) is at least 10% smaller than the cross-sectional area A_d of segment d), and the cross-sectional area A_c of the segment c) is at least 10% greater than the cross-sectional area A_c of segment e).
- 2. A dividing wall column as claimed in claim 1, wherein the cross-sectional area A_b of the segment b) is at least 40%, preferably at least 60%, smaller than the cross-sectional area A_d of segment d).
- 3. A dividing wall column as claimed in claim 1, wherein the cross-sectional area $\rm A_{\rm c}$ of

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the segment c) is at least 40%, preferably at least 60%, greater than the cross-sectional area of segment e).

- 4. A dividing wall column as claimed in claim 1, wherein the dividing wall is arranged obliquely between the segments f) and g) and forms an angle of from 25 to 75°, preferably from 55 to 65°, to the horizontal.
- 5. A dividing wall column as claimed in claim 1, wherein the operating pressure P is in the range from 0.0005 to 10 bar and the calculated ratios of the cross-sectional areas A'_b/A'_d and A'_c/A'_e are given by the following relationships

$$\frac{\mathbf{A'_b}}{\mathbf{A'_d}} = \left(\frac{\mathbf{m_{s,b}}}{\mathbf{m_{s,d}}}\right) \times \left(\frac{\mathbf{m_{i,b}}}{\mathbf{m_{i,d}}}\right)^{\mathbf{C}}$$

$$\frac{\mathbf{A'_c}}{\mathbf{A'_e}} = \left(\frac{\mathbf{m_{s,c}}}{\mathbf{m_{s,e}}}\right) \times \left(\frac{\mathbf{m_{i,c}}}{\mathbf{m_{i,e}}}\right)^{\mathbf{C}}$$

where A'_b , A'_d , A'_c , A_e are the cross-sectional areas of the segments b,d,c,e provided for the calculation; $m_{s,b}$, $m_{s,d}$, $m_{s,c}$, $m_{s,e}$ are the volume flows of gas through the segments b,d,c,e, measured in m^3 /h; $m_{i,b}$, $m_{i,d}$, $m_{i,c}$, $m_{i,e}$ are the volume flows of liquid through the segments b,d,c,e, measured in m^3 /h, and the exponent C is obtained as operating-pressure-dependent variable from the empirically determined function shown in Fig. 3, and the cal- culated ratios A'_b/A'_d and A'_c/A'_e deviate from the corresponding, actual ratios A_b/A_d and A_c/A_e by not more than 30%, preferably not more than 20%.

6. A dividing wall column as claimed in claim 1, where- in the operating pressure is

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from 0.0005 to 0.02 bar and liquid distributors in which the liquid predistribution occurs by the bank-up principle and the downstream fine liquid distribution occurs by the capillary principle are used.

- 7. A dividing wall column as claimed in claim 1, wherein ordered packing having a cross-channel structure is used as separation-active internals.
- 8. A dividing wall column as claimed in claim 1, wherein ordered packing having a cross-channel structure is used as separation-active internals and the uppermost layer of packing below the liquid distributor is aligned so that the individual layers are aligned parallel to the dividing wall.
- 9. A process for isolating pure ethylhexyl p-methoxy- cinnamate by distillation using a dividing wall column as claimed in <u>any of claims 1 to 8</u>, wherein the feed mixture introduced comprises from 70 to 95%, preferably from 75 to 90%, of ethylhexyl p-methoxycinnamate as intermediate-boiling desired product.

